

2014

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This document is the authors' final version of the published article.

Link to published article: <http://dx.doi.org/10.1038/srep06386>

APA Citation

Chen, J., Ng, J., Ding, K., Fung, K., Lin, Z., & Chan, C. (2014). Negative optical torque. *Scientific Reports*, 4, 6386. <https://doi.org/10.1038/srep06386>

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Negative Optical Torque

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SUBJECT AREAS:

OPTICAL MANIPULATION
AND TWEEZERS

COMPUTATIONAL
NANOTECHNOLOGY

Received
8 May 2014

Accepted
6 August 2014

Published
17 September 2014

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Light carries angular momentum, and as such it can exert torques on material objects. Applications of these opto-mechanical effects were limited initially due to their smallness in magnitude, but later becomes powerful and versatile after the invention of laser. Novel and practical approaches for harvesting light for particle rotation have since been demonstrated, where the structure is always subjected to a positive optical torque along a certain axis if the incident angular momentum has a positive projection on the same axis. We report here an interesting phenomenon of “negative optical torque”, meaning that incoming photons carrying angular momentum rotate an object in the opposite sense. Surprisingly this can be realized quite straightforwardly in simple planar structures. Field retardation is a necessary condition and discrete rotational symmetry of material object plays an important role. The optimal conditions are explored and explained.

The negative optical torque (NOT) phenomenon manifestly conserves angular momentum^{1–4}. Let us consider an object illuminated by an electromagnetic wave carrying a z -component angular momentum of L_z^{inc} . After being scattered by the object, the total z -component angular momentum of the light is L_z^{sca} . If the consequence of scattering is such that $L_z^{sca} > L_z^{inc}$, then angular momentum conservation requires that the difference $L_z^{sca} - L_z^{inc}$ must be balanced by a NOT acting on the object. Consequently, negative optical torque is consistent with total angular momentum conservation. The question is then whether such phenomenon, which does not violate conservation laws, can be realized in practice. If so, is NOT easily observable? We will show that NOT is in fact ubiquitous, as it can be realized in many transparent or weakly absorptive structures, in discrete rotationally symmetric or even irregular structures, and also in planar or even 3D structures. We shall show that field retardation is necessary for achieving NOT and discrete rotational symmetry enhances NOT. The realization of NOT adds new possibility to the existing novel^{5–12} and practical^{13–21} technique of optical rotation. It may open up new applications in areas where optical micromanipulation play a role^{22,23}. We note that although negative optical torque here is indeed the angular counterpart of optical pulling force^{24–27}, it is definitely not a straight forward corollary. For example, symmetry is not a key factor in achieving optical pulling force but it proved to be of considerable importance in realizing NOT. Also, NOT is ubiquitous while optical pulling force can only be observed with a carefully chosen combination of beam profile and particle properties.

Results

Explicit numerical demonstration of negative optical torque. Explicit examples of structures where NOT can be realized are shown in Fig. 1. For the ease and accuracy of computation and interpretation, we consider planar structures composing of dielectric microspheres located on the xy -plane. The axis for which the torque is to be calculated is parallel to the z -axis and goes through the center of mass marked in Fig. 1, where some of the structures possess discrete rotational symmetry but some do not. We stress that our conclusions are valid not only for discrete system comprising of spheres, but also to a continuous piece of material.

The time-averaged optical torque Γ acting on the concerned structure is computed by (see Methods)

$$\Gamma = \iint_{\sigma} (\mathbf{r} \times \langle \vec{\mathbf{T}} \rangle) \cdot \hat{\mathbf{n}} dS. \quad (1)$$

where the time averaged Maxwell stress tensor is given by²⁸

$$\langle \vec{\mathbf{T}} \rangle = \frac{\epsilon_0}{2} \left[\mathbf{E}\mathbf{E}^* + c^2 \mathbf{B}\mathbf{B}^* - \frac{1}{2} (|\mathbf{E}|^2 + c^2 |\mathbf{B}|^2) \mathbf{I} \right], \quad (2)$$

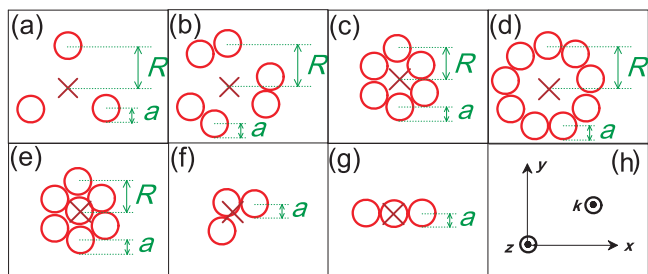


Figure 1 | Examples of planar structures that can realize negative optical torque. (a)–(g) structures composed of an array of identical dielectric spheres. R (a) is the structure (sphere) radius. The crosses mark the centers of mass, which coincides with the axis of rotation. (h) shows the coordinate system. The incident plane wave has a k -vector (k) along the z -axis.

the origin of the coordinate system is chosen to be the center of mass marked in Fig. 1, σ is any surface that encloses the entire structure, and \mathbf{r} is the position vector originating from the center of mass. Irrespective of the structural orientation and morphology, the z -component optical torque calculated by Eq. (1) can be written as

$$\Gamma_z = \sum_{m_i} \frac{m_i \hbar}{\hbar \omega} W_{ext}^{(m_i)} - \sum_m \frac{m \hbar}{\hbar \omega} W_{sca}^{(m)}, \quad (3)$$

where ω is the angular frequency of incident wave, and m_i and m characterize, respectively, the azimuthal channels for the incident and scattered waves. $W_{ext}^{(m_i)}$ is the energy extinction rate for incident wave from channel m_i , and $W_{sca}^{(m)}$ is the rate at which energy is scattered into the outgoing channel m . The derivation and the explicit expressions of $W_{ext}^{(m_i)}$ and $W_{sca}^{(m)}$ are given in the Methods section. As long as the scattering problem can be treated accurately, Eq. (3) is exact within the framework of classical electrodynamics. In the numerical results shown below, we will consider objects composing of an array of spheres as our prototypical system because the scattering problem can be solved numerically using the generalized Mie theory for multi-sphere to a very high precision. This removes any doubt that the NOT effects observed are numerical artifacts. And unless stated otherwise, the incident wave is a left circularly polarized²⁸ plane wave propagating along the z -axis, with a positive angular momentum and an intensity of 1 mW/ μm^2 .

Figure 2 shows the calculated optical torques versus ka for three morphologically different planar structures with different types of incident waves, where k is the wave number and a is the radius of the comprising spheres. The results clearly show that NOT can be realized in all three structures, which include planar triangular or hexagonal structures consisting of silicon or polystyrene microspheres, illuminated by a circularly polarized plane wave, Gaussian beam, or Laguerre Gaussian beam. The optical torques can take negative values at some intervals of ka . The three structures in Fig. 2 are not of special design. Other planar structures can serve the same purpose. Figure 2 illustrates that NOT can be quite universal: it can be observed in different structures (planar or non-planar) with different forms of incident wave, including plane wave, Gaussian beam, and Laguerre Gaussian beam. For the Laguerre Gaussian beam, the smaller structure (yellow line) do not experience a NOT as the beam cannot probe the structural details. While for the larger structure (blue line), NOT is still seen.

Analytical demonstration of negative optical torque and the role of retardation. In addition to numerical demonstration, formal analytical understanding of NOT can be developed by considering the following prototypical system: a pair of non-absorbing dipolar spheres located on the xy -plane, illuminated by a z -propagating plane wave with arbitrary polarization. Following Ref. 24 and

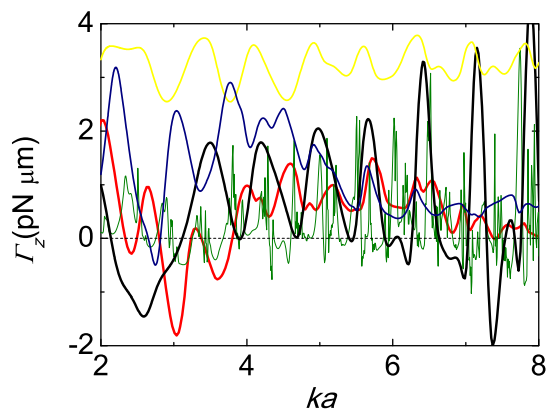


Figure 2 | Optical torque for different structures under different incident waves carrying positive angular momentum. Red: Optical torque versus varying k for Fig. 1(e) ($\epsilon_r = 2.46$, $a = 0.49 \mu\text{m}$, $R = 1.0 \mu\text{m}$) illuminated by a left circularly polarized plane wave of intensity 1 mW/ μm^2 . Green: Optical torque versus varying a for Fig. 1(a) composed of silicon spheres ($\epsilon_r = 12.6096$, $R = 1.16a$, $\lambda = 1064 \text{ nm}$) in water illuminated by a left circularly polarized plane wave of intensity = 1 mW/ μm^2 . Black: Optical torque versus varying k for Fig. 1(a) ($\epsilon_r = 2.4649$, $a = 0.5 \mu\text{m}$, $R = 0.58 \mu\text{m}$) illuminated by a left circularly polarized Gaussian beam (numerical aperture = 0.9 and total power = 0.05 W). Yellow: Optical torque versus k for Fig. 1(a) ($\epsilon_r = 2.4649$, $a = 0.5 \mu\text{m}$, $R = 0.58 \mu\text{m}$) illuminated by a linearly polarized 10 mW Laguerre–Gaussian beam with topological charge of 1 and a N.A. of 0.9. Blue: Optical torque versus k for Fig. 1(e) ($\epsilon_r = 2.4649$, $a = 0.49 \mu\text{m}$, $R = 1.0 \mu\text{m}$) illuminated by a linearly polarized 10 mW Laguerre–Gaussian beam with topological charge of 1 and a N.A. of 0.9. Negative torque ($\Gamma_z < 0$) means that the light beam induces the object to rotate in the opposite sense as the angular momentum of the incident photon.

retaining only the electric dipole term, one can derive the formula for optical torque:

$$\Gamma_z = \frac{|\alpha|^2}{2} \text{Re}(\mu_{\parallel} - \mu_{\perp}) \left[\frac{\text{Re}(E_{\parallel} E_{\perp}^*) \text{Re}(1 + \alpha \mu_{\perp} + \alpha \mu_{\parallel})}{+ (|E_{+}|^2 - |E_{-}|^2) \text{Im}(\alpha \mu_{\parallel} - \alpha \mu_{\perp})} \right], \quad (4)$$

where

$$\begin{aligned} \mu_{\parallel} &= \frac{2e^{ikR}}{4\pi\epsilon_0 R^3} (1 - ikR), \\ \mu_{\perp} &= \frac{e^{ikR}}{4\pi\epsilon_0 R^3} (k^2 R^2 + ikR - 1) \end{aligned} \quad (5)$$

are the eigenvalues of the dyadic Green's function²⁹, R is the separation between the dipoles, and α is the dipolar polarizability. E_{\parallel} and E_{\perp} are the projection of the electric field parallel to or perpendicular to the particle axis (i.e. the amplitudes of linear polarization), E_{+} and E_{-} are the amplitudes of left and right circularly polarized components. The effect of field retardation manifests itself as a factor of e^{ikR} in the expression of μ_{\parallel} and μ_{\perp} , leading to oscillatory behavior of torque versus kR . We shall see that it is this oscillation due to retardation that opens up the possibility of NOT.

The first term in Eq. (4) is proportional to $\text{Re}(E_{\parallel} E_{\perp}^*)$. It is an aligning force, which vanishes for circular polarization. For linearly polarization, it vanishes only when either $E_{\parallel} = 0$ or $E_{\perp} = 0$, corresponding to the case of polarization being perpendicular or parallel to the particle axis, respectively. Accordingly, depending on kR , this force tries to align the particle chain to a direction that is either perpendicular or parallel to the polarization.

The second term in Eq. (4), which is proportional to $(|E_{+}|^2 - |E_{-}|^2)$, also has a simple interpretation: the sign of the corresponding



torque is determined by the competition between the amplitudes of the left and right circular polarization. Consequently, it is a rotating force that will keep the object turning. Depending on kR , a left circularly polarized light can induce a positive or negative torque. Consequently, this term is responsible for NOT. Moreover, the term vanishes identically for linear polarization.

The two terms in Eq. (4) are competing with each other. When the incident wave is predominantly linearly polarized, the first aligning term will be dominating and the particle chain will be aligned. On the other hand, for circular polarization, the second turning term will dominate and the particle chain will be set into rotation. Equation (4) contains many salient features of light induced torque. For circular polarization, it becomes

$$\Gamma_z = \frac{|\alpha^2|}{2} (|E_+|^2 - |E_-|^2) f_1 [\text{Im} \alpha + |\alpha| \sin(2kR + \delta)], \quad (6)$$

where $\Gamma_x = \Gamma_y = 0$ by symmetry,

$$f_1 = \frac{k^4 R^4 + 3k^2 R^2 + 9}{32\pi^2 R^6 \epsilon_0^2}, \quad (7)$$

and

$$\delta = \tan^{-1} \left[\frac{(6k^3 R^3 - 18kR) \text{Re}\{\alpha\} + (9 - 15k^2 R^2 + k^4 R^4) \text{Im}\{\alpha\}}{(9 - 15k^2 R^2 + k^4 R^4) \text{Re}\{\alpha\} - (6k^3 R^3 - 18kR) \text{Im}\{\alpha\}} \right]. \quad (8)$$

The first term inside the square bracket of Eq. (6) corresponds to a positive bias, whereas the second term carrying $\sin(2kR + \delta)$ oscillates between positive and negative values due to the spatial field retardation associated with a finite value of kR . Since $|\alpha| > \text{Im} \alpha$, the amplitude of oscillation is larger than that of the bias, accordingly, the optical torque can sometimes be negative due to spatial retardation induced oscillation. This simple exercise not only demonstrates analytically the possible existence of NOT, the results also show that field retardation is essential to realize NOT.

For very small separations between the dipoles and a left circularly polarized incident wave, Eq. (6) asymptotically approaches

$$\Gamma_z = |\alpha^2| E_0^2 \frac{9 \text{Im} \alpha}{32\pi^2 \epsilon_0^2 R^6}. \quad (9)$$

Since $\text{Im} \alpha > 0$ by optical theorem³⁰, $\Gamma_z > 0$. This result is not surprising. In the long wavelength limit ($kR \ll 1$), the wave cannot probe the details of the structure. Therefore the sign of the torque must be the same as that of the incident wave. In fact, this conclusion holds true for any small structures, as we shall see in the following sessions.

Physical origin of the negative optical torque. We now analyze the physical origin of NOT for more general structures. Equation (3) allows for a heuristic physical interpretation: $W_{\text{ext}}^{(m_i)}/\hbar\omega$ is the extinction rate for incoming photons from channel m_i , and each of these photons carries $m_i\hbar$ of angular momentum, therefore the rate at which the object acquires angular momentum from all azimuthal channels of the incident beam is given by the first term in Eq. (3). Similarly $W_{\text{sca}}^{(m)}/\hbar\omega$ is the rate of photons being scattered into channel m , and each of these photons gives a recoil angular momentum of $-m\hbar$, therefore the rate at which the object obtains angular momentum due to recoil is given by the second term in Eq. (3). Equation (3) also shows that the transfer of angular momentum can be interpreted as occurring in two steps. First, the photons are intercepted by the scatterer. This induces an extinction torque given by the first term in Eq. (3). For an incident wave consisting of solely positive m_i components, this extinction torque is positive definite. So if NOT exists at all, it must come from the recoil torque in Eq. (3). Depending on the material and the structural properties of the object, some of the intercepted photons will be absorbed, while some will be scattered. The scattered photons exert a recoil torque on the object, as

given by the second term in Eq. (3), where $m < 0$ ($m > 0$) represent a positive (negative) contribution. If the negative contribution dominates, we will have a NOT.

The role of symmetry. Symmetry is the explanation to why the negative optical torque effect can actually be quite universal. Light cannot exert an optical torque on a transparent object possessing continuous rotational symmetry, since photons scattered by such an object preserve their angular momentum. From this point of view, the phenomenon of optical torque is a consequence of broken rotational symmetry. NOT is therefore inevitably tied to the symmetry of the structure and incident wave.

To see this, it suffices to consider objects with discrete rotational symmetry of degree m_s and for an incident wave with a single azimuthal channel $m_i > 0$. In wave scattering theory, based on irreducible tensor approach, wave can be decomposed into modes characterized by two mode indices: total angular momentum index l , termed also angular momentum channel index, and z-component of angular momentum index m , termed also azimuthal channel index in this paper. We will see that it is discrete rotational symmetry that allows NOT to be observed ubiquitously.

The angular momentum selection rule for photons after being scattered by such object is

$$m = m_i + n \times m_s, \quad (10)$$

where m is an allowed channel for the scattered wave and $n = 0, \pm 1, \pm 2$ and so on^{31,32} (see part 1 of Methods for a proof). Equation (10) is the angular counterpart of the grating effect for a periodic surface illuminated by a plane wave. Although Eq. (10) is analogous to linear grating (periodic in space), the rules are correct for all structures in the rotational case because any structure is invariant under a rotation of 2π . With Eq. (10), the z-component optical torque of Eq. (3) can be re-written as

$$\Gamma_z = \frac{m_i \hbar}{\hbar\omega} W_{\text{ext}}^{(m_i)} - \sum_n (m_i + n \times m_s) \frac{\hbar}{\hbar\omega} W_{\text{sca}}^{(m_i + n \times m_s)}. \quad (11)$$

In principle, the positive and negative n channels contribute to NOT and positive optical torque (POT), respectively, while the $n = 0$ channel, representing no change in the angular momentum of the photons, produces no torque. However, the contribution for channels with $|m| \gg kR$ can be rather weak. When $|m| \gg kR$, the centrifugal effect forces the amplitude of the mode m to decrease rapidly for region where $R < |m|/k$ ³³. There is very little overlap between the mode m and the object, forbidding the object to scatter wave into these channels. Consequently, these channels contribute negligibly to optical torque.

If m_s is very large, the condition of $|m| \gg kR$ will be met for all channel except the $n = 0$ channel, even for the low order modes with $n = \pm 1$. In fact, continuous rotational symmetry is an idealization rather than reality. An object with very fine sub-wavelength details (such as a small object with a large m_s) that is beyond the diffraction limited resolving power of the incoming wave can be thought to have continuous rotational symmetry as far as light scattering is concerned. In this case, the contributions from all channels become vanishingly small except the $n = 0$ channel. Therefore the wave exerts vanishingly small torque on such object with high discrete rotational symmetry and relatively small size, just like a structure with continuous rotational symmetry. The incident wave m_i can only be scattered into the azimuthal channel characterized by the same m_i . Equation (3) thus reduces to $\Gamma_z = \sum_{m_i} m_i \hbar W_{\text{abs}}^{(m_i)}/\hbar\omega$, where

$W_{\text{abs}}^{(m_i)} = W_{\text{ext}}^{(m_i)} - W_{\text{sca}}^{(m_i)}$ is proportional to the energy absorption rate in channel m_i . Since both $W_{\text{abs}}^{(m_i)}$ and m_i are positive definite, it follows that $\Gamma_z \geq 0$.



In the other extreme situation of $m_s \ll m_i$, according to Eq. (3), the torque is positive definite as

$$\begin{aligned} \Gamma_z &\approx m_i / \omega \left(W_{ext}^{(m_i)} - \sum_n W_{sca}^{(m_i+n \times m_s)} \right) \\ &= m_i \frac{(W_{ext} - W_{sca})}{\omega} = \frac{m_i W_{abs}}{\omega} \geq 0, \end{aligned} \quad (12)$$

where $W_{abs} = (W_{ext} - W_{sca})$ is the rates at which energy is absorbed.

If NOT can exist, it must be for some moderate value of $m_s < kR$ so that the corresponding partial waves can reach the scatterer to transfer angular momentum. This is in fact a manifestation of the optical diffraction limit. If the small structure has some very fine sub-wavelength details, such as patterns with high degree of rotational symmetry located in a small region, the incident wave will not be able to probe them. Thus the information on the symmetry will be lost, eliminating the possibility of observing NOT. In general, NOT can be easily observed if $m_s < l_{max}$, where $l_{max} = kR + 4.05(kR)^{1/3} + 2$ is an empirical formula for the angular momentum truncation order of the scatterer^{31,32}.

Next, we argue that a larger m_s favors NOT as long as $|m|$ is not significantly larger than kR . In Fig. 3, the optical torque acting on objects composing of the same type of spheres but with different values of m_s ($m_s = 1, 2, 3$) are shown. By comparing $m_s = 1$ to $m_s = 3$, one sees that NOT is more easily observed for a larger value of m_s . These can be explained as follows. We note that according to our simulations, and also Eq. (6), the total torque consists of a positive bias part and an oscillatory part. It is the oscillatory part that gives NOT. For the object with $m_s = 1$ (red line), the torque acting on all three spheres are different. Therefore the negative torque acting on one sphere may be canceled by the positive torque acting on another. This weakens the oscillatory part of the total torque and reduces the possibility of NOT. For the object with $m_s = 3$ (blue line), the torque acting on each sphere is the same by symmetry, so the torques reinforce each other rather than cancel each other. This preserves the strength of the oscillatory part of the total torque and allows NOT to be observed more easily. More discussion about the role of symmetry can be found in the Supplementary Information.

Discussion

For the more complex systems we have considered (arrays of spheres as shown in Fig. 1), we further argue here that spatial retardation is also essential for NOT, as in the simple example we discussed in the previous section. We show in Fig. 4 the optical torque due to indi-

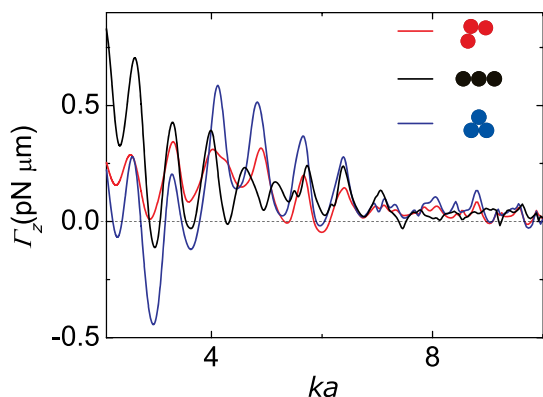


Figure 3 | Optical torque versus ka for objects with different discrete rotational symmetry. The objects are composed of identical dielectric spheres ($\epsilon_r = 2.4649$). The red, black, and blue lines correspond to $m_s = 1, 2$, and 3 , respectively. The degree of discrete rotational symmetry is seen to significantly enhance negative optical torque (i.e. higher m_s favors negative torque).

vidual azimuthal channel for structures with three-fold ($m_s = 3$) or six-fold ($m_s = 6$) rotational symmetry. According to Eq. (10), for three-fold symmetric structures showed in Fig. 4(a)–(b), light is scattered into azimuthal channels characterized by $m = 3n + 1$, where $n = 0, \pm 1, \pm 2, \dots$ etc. The $m = 1$ channel [i.e. $n = 0$ in Eq. (10)] does not contribute to torque for lossless spheres. Light scattered into azimuthal channels $m = -2, -5, -8$ and so on will contribute to positive optical torque, whereas the channels characterized by $m = 4, 7, 10$ and so on will induce NOT. As multiple scattering is not strong in dielectrics, the recoil torque is dominated by $n = \pm 1$, corresponding to $m = m_i \pm m_s = -2$ or 4 . In Fig. 4 the oscillatory behavior of the torques due to individual partial waves versus wavelength and structural size is the signature of retardation, while the peaks for $n = \pm 1$ channels correspond to Mie type resonance. It is precisely due to this retardation induced oscillation that the total torque takes positive or negative value. The situation for the six-fold symmetric structures showed in Fig. 4(c)–(d) is similar.

Finally, we argue that small object does not favor NOT. Consider, for example, a small three-fold ($m_s = 3$) rotationally symmetric lossless structure illuminated by a left circularly polarized plane wave ($m_i = 1$). If the structure is small such that wave components with higher angular momentum cannot reach the scatterer and the truncation angular momentum index $l_{max} = 1$, then the torque is approximately equal to zero since only $n = 0$ term appears in Eq. (11). As the size of the structure increases such that we have to take $l_{max} = 2$, the second term in the series (corresponding to $n = -1$) is now significant, which is given by (see Methods for the definition of partial torque τ_m that is due to each individual outgoing azimuthal channel m)

$$\tau_{-2} = m_s W_{-2,2} / \omega. \quad (13)$$

Equation (13) is positive definite and therefore corresponds to POT. One then expects that a small scatterer cannot experience a NOT. If we consider larger particle, NOT will become possible. For example, the third term in the series (corresponding to $n = 1$) is given by

$$\tau_4 = -m_s W_{4,4} / \omega, \quad (14)$$

which, when larger in magnitude than τ_{-2} in Eq. (13), results in negative total torque.

In summary, we showed that negative optical torque is ubiquitous in simple configurations and can be induced by a broad class of incident waves. We note that while negative optical torque can be viewed as the angular counterpart of the optical pulling force, the conditions under which the “negative response” can be realized are very different. The optical pulling force is achievable only for special kinds of optical beams acting on some specific particles^{24–27} whereas NOT can be realized rather easily. NOT can occur if the recoil torque happens to be negative and larger in magnitude than the extinction torque, which is made possible by retardation effects and enhanced by discrete rotational symmetry. We remark that our theory is valid for both spin and orbital angular momentum (i.e. arbitrary m_i) of light.

Methods

Derivation of the azimuthal mode selection rule in electromagnetic scattering. We shall prove that when an incident wave characterized by a single azimuthal number m_i ^{30,32} impinges on a structure with m_s -fold rotational symmetry, it will be scattered into azimuthal channels given by the azimuthal mode selection rule in Eq. (10).

Let us start with the total electric field for a general scattering problem, which is given by the Lippmann-Schwinger integral equation^{34,35}

$$\mathbf{E}(\mathbf{r}) = \mathbf{E}_{inc}(\mathbf{r}) + \int \tilde{\mathbf{G}}(\mathbf{r}, \mathbf{r}') [\epsilon_r(\mathbf{r}') - 1] k^2 \mathbf{E}(\mathbf{r}') d\mathbf{r}', \quad (15)$$

where $\mathbf{E}_{inc}(\mathbf{r})$ denotes the incident electric field, $\epsilon_r(\mathbf{r}')$ is the position dependent relative dielectric constant, and $k = \omega/c$ is the wave number in the background. The second term on the right hand side of Eq. (15) gives the scattered field:

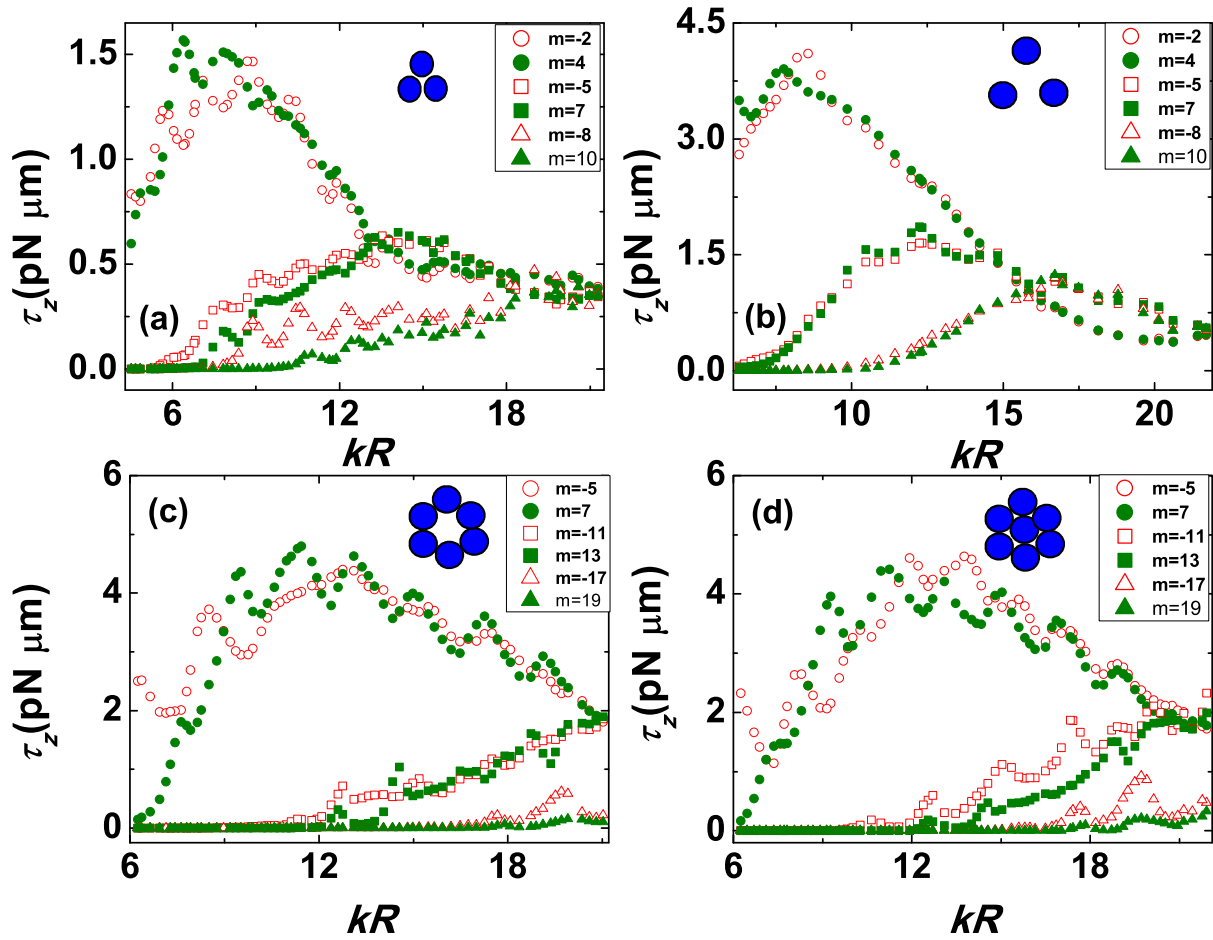


Figure 4 | The contribution (in absolute value) to the torque by individual partial wave azimuthal channels versus kR . (a)–(b) three-fold and (c)–(d) six-fold rotationally symmetric dielectric structures ($\epsilon_r = 2.4649$, $a = 0.49 \mu\text{m}$). The incident field is a left circularly polarized plane wave (intensity is $1 \text{ mW}/\mu\text{m}^2$). $R = 0.58 \mu\text{m}$ for (a) and $R = 1 \mu\text{m}$ for (b)–(d). The oscillations are due to spatial retardation.

$$\mathbf{E}_{\text{sca}} = \int \vec{\mathbf{G}}(\mathbf{r}, \mathbf{r}') \cdot [\epsilon_r(\mathbf{r}') - 1] k^2 \mathbf{E}(\mathbf{r}') d\mathbf{r}', \quad (16)$$

where $\vec{\mathbf{G}}(\mathbf{r}, \mathbf{r}')$ is the free-space dyadic Green's function²⁹, which can be written as

$$\vec{\mathbf{G}}(\mathbf{r}, \mathbf{r}') = \sum_{\alpha, l, m} a_{\alpha mn} \mathbf{O}_{\alpha ml}(r, \theta, \phi) \mathbf{O}_{\alpha(-m)l}(r', \theta', \phi'), \quad (17)$$

where $\mathbf{O}_{\alpha mn}$ represents vector spherical wave functions \mathbf{M}_{mn} , \mathbf{N}_{mn} and \mathbf{L}_{mn} ^{29,36} for $\alpha = 1, 2$, and 3 , respectively. The ϕ -dependent part of $\mathbf{O}_{\alpha ml}(r, \theta, \phi)$ is of the form $e^{im\phi}$ and similarly $\mathbf{O}_{\alpha(-m)l}(r', \theta', \phi')$ depends on ϕ' through $e^{-im\phi'}$. As a result, each term characterized by m in the dyadic Green function $\vec{\mathbf{G}}(\mathbf{r}, \mathbf{r}')$ given by Eq. (17) shows $e^{im(\phi-\phi')}$ azimuthal dependence.

Inserting Eq. (15) into Eq. (16), we arrive at

$$\begin{aligned} \mathbf{E}_{\text{sca}} = & \int \vec{\mathbf{G}}(\mathbf{r}, \mathbf{r}') \cdot [\epsilon_r(\mathbf{r}') - 1] k^2 \mathbf{E}_{\text{inc}}(\mathbf{r}') d\mathbf{r}' \\ & + \int \int \vec{\mathbf{G}}(\mathbf{r}, \mathbf{r}') \cdot \vec{\mathbf{G}}(\mathbf{r}', \mathbf{r}'') \cdot [\epsilon_r(\mathbf{r}') - 1][\epsilon_r(\mathbf{r}'') - 1] k^4 \mathbf{E}_{\text{inc}}(\mathbf{r}'') d\mathbf{r}' d\mathbf{r}'' \\ & + \dots, \end{aligned} \quad (18)$$

where \dots denotes higher order scattering terms. Note that the azimuthal dependence of the incident wave $\mathbf{E}_{\text{inc}}(\mathbf{r}')$ on ϕ' is given by $e^{im_s\phi'}$, while for a structure with m_s -fold symmetry, the dielectric constant may be expanded in a Fourier series

$$\epsilon_r(\mathbf{r}') - 1 = \sum_{n=-\infty}^{\infty} A_n e^{inm_s\phi'}. \quad (19)$$

Therefore, for the first term on the right hand side of Eq. (18), the integration over azimuthal coordinate ϕ' reads

$$\sum_{\alpha, l, m} \dots \int_0^{2\pi} e^{-im\phi'} \left(\sum_n A_n e^{inm_s\phi'} \right) e^{im_i\phi'} d\phi',$$

which requires $m = m_i + nm_s$ in order to have a non-zero contribution to \mathbf{E}_{sca} . Similarly, for the second term on the right hand side of Eq. (18), the integration over ϕ' and ϕ'' can be written as

$$\sum_{\alpha, l, m} \sum_{\alpha', l', m'} \dots \int_0^{2\pi} \int_0^{2\pi} e^{-im\phi'} e^{im'(\phi' - \phi'')} \left(\sum_{n, n'} A_n e^{inm_s\phi'} A_{n'} e^{in'm_s\phi''} \right) e^{im_i\phi''} d\phi' d\phi''.$$

It then follows straightforwardly that the non-vanishing terms should satisfy $m' = m_i + n'm_s$ and $m = m' + nm_s$, implying that only azimuthal modes with $m = (n + n')m_s + m_i$ survive in the scattered field.

The procedure applies straightforwardly to higher order scattering terms in Eq. (18), leading to the conclusion that the scattered field contains only azimuthal modes with m satisfying $m = m_i + nm_s$, where n is an integer. This is actually an angular analogue of the much better known phase matching condition for a surface of periodic lattice derived from Floquet's theorem.

The contribution of individual azimuthal channel to optical torque. The time-averaged optical torque $\langle \Gamma \rangle_t$ acting on a scatterer is obtained from the surface integration of the time-averaged angular momentum flux tensor $\langle \vec{\mathbf{K}} \rangle_t$ by

$$\langle \Gamma \rangle_t = - \iint_{\sigma} \mathbf{n} \cdot \langle \vec{\mathbf{K}} \rangle_t dS = - \iint_{\sigma} \mathbf{n} \cdot (\langle \vec{\mathbf{T}} \rangle_t \times \mathbf{r}) dS, \quad (20)$$

where σ can be any surface that encloses the entire scatterer, and \mathbf{n} denotes the unit outward normal at surface σ . The time-averaged Maxwell stress tensor $\langle \vec{\mathbf{T}} \rangle_t$ is given by

$$\langle \vec{\mathbf{T}} \rangle_t = \frac{1}{2} \text{Re}[\epsilon_0 \mathbf{E}_c \mathbf{E}_c^* + \mu_0 \mathbf{H}_c \mathbf{H}_c^* - \frac{1}{2} (\epsilon_0 \mathbf{E}_c \cdot \mathbf{E}_c^* + \mu_0 \mathbf{H}_c \cdot \mathbf{H}_c^*) \vec{\mathbf{I}}], \quad (21)$$

where ϵ_0 and μ_0 are, respectively, the permittivity and permeability in free space, and $\vec{\mathbf{I}}$ is the unit tensor. The electric (magnetic) field \mathbf{E}_c (\mathbf{H}_c) is a sum of incident field \mathbf{E}_i (\mathbf{H}_i)



and scattered field \mathbf{E}_s (\mathbf{H}_s), namely, $\mathbf{E}_e = \mathbf{E}_i + \mathbf{E}_s$ and $\mathbf{H}_e = \mathbf{H}_i + \mathbf{H}_s$. These can be expanded in terms of vector spherical wave functions (VSWFs)^{37,38}:

$$\begin{aligned}\mathbf{E}_i &= -\sum_{l=1}^{\infty} \sum_{m=-l}^l iE_{ml} [p_{ml} \mathbf{N}_{ml}^{(1)}(\mathbf{k}, \mathbf{r}) + q_{ml} \mathbf{M}_{ml}^{(1)}(\mathbf{k}, \mathbf{r})], \\ \mathbf{H}_i &= -\frac{k}{\omega\mu} \sum_{l=1}^{\infty} \sum_{m=-l}^l E_{ml} [q_{ml} \mathbf{N}_{ml}^{(1)}(\mathbf{k}, \mathbf{r}) + p_{ml} \mathbf{M}_{ml}^{(1)}(\mathbf{k}, \mathbf{r})], \\ \mathbf{E}_s &= \sum_{l=1}^{\infty} \sum_{m=-l}^l iE_{ml} [a_{ml} \mathbf{N}_{ml}^{(3)}(\mathbf{k}, \mathbf{r}) + b_{ml} \mathbf{M}_{ml}^{(3)}(\mathbf{k}, \mathbf{r})], \\ \mathbf{H}_s &= \frac{k}{\omega\mu} \sum_{l=1}^{\infty} \sum_{m=-l}^l E_{ml} [b_{ml} \mathbf{N}_{ml}^{(3)}(\mathbf{k}, \mathbf{r}) + a_{ml} \mathbf{M}_{ml}^{(3)}(\mathbf{k}, \mathbf{r})],\end{aligned}\quad (22)$$

where $E_{ml} = |E_0|^l \gamma_{ml}^{1/2}$ and $\gamma_{ml} = \frac{2l+1}{l(l+1)} \frac{(l-m)!}{(l+m)!}$. The expansion coefficients p_{ml} and q_{ml} (a_{ml} and b_{ml}) are known as partial wave expansion coefficients for incident (scattered) waves. Here, p_{ml} and q_{ml} can be obtained from an overlap integral between the incident field and VSWFs. For a collection of spheres a_{ml} and b_{ml} can be obtained by solving the scattering problem using the generalized Mie theory for multispheres.

By the orthogonality of the VSWFs, the integration in Eq.(20) can be worked out analytically (for an arbitrary incident field) at a surface far away from the scatterer to give the z -component Γ_z of the time-averaged optical torque,

$$\Gamma_z = \frac{2\pi\epsilon_0 |E_0|^2}{k^3} \sum_{l=1}^{\infty} \sum_{m=-l}^l m \text{Re} [p_{ml} a_{ml}^* + q_{ml} b_{ml}^* - (|a_{ml}|^2 + |b_{ml}|^2)]. \quad (23)$$

On the other hand, with the incident and scattered field expanded in terms of VSWFs, the rate W_{sca} at which incident wave energy is scattered and the rate W_{ext} at which the energy is intercepted can be written as, see, e.g., Ref. 38

$$\begin{aligned}W_{sca} &= -\iint_{\sigma} \mathbf{n} \cdot \langle \mathbf{P}_{sca} \rangle_t dS = \sum_m W_{sca}^{(m)}, \\ W_{ext} &= -\iint_{\sigma} \mathbf{n} \cdot \langle \mathbf{P}_{ext} \rangle_t dS = \sum_m W_{ext}^{(m)},\end{aligned}\quad (24)$$

where

$$\begin{aligned}W_{sca}^{(m)} &= \frac{2\pi\epsilon_0 c |E_0|^2}{k^2} \sum_l (|a_{ml}|^2 + |b_{ml}|^2) \\ W_{ext}^{(m)} &= \frac{2\pi\epsilon_0 c |E_0|^2}{k^2} \sum_l \text{Re}(p_{ml} a_{ml}^* + q_{ml} b_{ml}^*),\end{aligned}$$

and the time-averaged Poynting vectors $\langle \mathbf{P}_{sca} \rangle_t$ and $\langle \mathbf{P}_{ext} \rangle_t$ are given by

$$\langle \mathbf{P}_{sca} \rangle_t = \frac{1}{2} \text{Re}[\mathbf{E}_s \times \mathbf{H}_s^*], \quad \langle \mathbf{P}_{ext} \rangle_t = \frac{1}{2} \text{Re}[\mathbf{E}_i \times \mathbf{H}_s^* + \mathbf{E}_s \times \mathbf{H}_i^*].$$

For an incident wave from a single azimuthal channel m_i , the partial wave expansion coefficients satisfy $p_{ml} = p_{mi} \delta_{mm_i}$ and $q_{ml} = q_{mi} \delta_{mm_i}$, where δ_{mm_i} is the Kronecker delta. So Eqs. (23) and (24), together with $W_{ext} = W_{sca}$ for lossless scatterer, imply that

$$\Gamma_z = \frac{2\pi\epsilon_0 |E_0|^2}{k^3} \left[\sum_{l,m} m_i (|a_{ml}|^2 + |b_{ml}|^2) - \sum_{l,m} m (|a_{ml}|^2 + |b_{ml}|^2) \right] \quad (25a)$$

$$= \frac{2\pi\epsilon_0 |E_0|^2}{k^3} \sum_{l,m} (m_i - m) (|a_{ml}|^2 + |b_{ml}|^2) \quad (25b)$$

$$= -\frac{m_s}{\omega} \sum_{n=-\infty}^{\infty} n \sum_{l=\max\{|m_i|, 1\}}^{\infty} W_{ml}, \quad (25c)$$

where $W_{ml} = \frac{2\pi\epsilon_0 c |E_0|^2}{k^2} (|a_{ml}|^2 + |b_{ml}|^2) > 0$ with $W_{sca} = \sum_{l,m} W_{ml}$, and $m = m_i + nm_s$ for a scatterer with m_s -fold rotational symmetry, see, Eq.(10). The first summation in Eq. (25a) corresponds to the extinction torque, which has the same sign as m_i , leading definitely to a POT, while the second summation in (25a) corresponds to recoil torque that can be positive or negative, since $m (= m_i + nm_s)$ and m_i may be of the same or opposite signs. Equation (25c) indicates that in order to exert an optical torque on a lossless object, the latter must scatter the incident wave into azimuthal channel m that differs from the incoming one m_i (such that $n \neq 0$). Based on Eq. (25c), one can separate the optical torque Γ_z into partial torque τ_m that is due to each individual azimuthal channel m of the scattered field

$$\Gamma_z = \sum_m \tau_m = \sum_n \tau_{m_i + nm_s}, \quad \tau_{m_i + nm_s} = -\frac{m_s n}{\omega} \sum_{l=\max\{|m_i|, 1\}}^{l_{\max}} W_{(m_i + nm_s)l}, \quad (26)$$

where l_{\max} is the truncation order for the angular momentum index in the infinite series. Equation(26) implies that all partial torques associated with positive (negative) n contribute to NOT (POT). The partial torques τ_m for some different allowed m_s (with $n = \pm 1, \pm 2, \pm 3$) are shown in Fig. 4 for the case where a left circularly plane wave (with $m_i = 1$) impinges on scatterers with $m_s = 3$ and 6. From Fig. 4, it is found that the absolute values of partial torque due to the same $|n|$ are quite close, since they contain roughly the same number of terms according to Eq.(26). In particular, all terms show oscillatory behavior versus kR due to field retardation. It is this retardation-induced oscillatory behavior that gives rise to the competition between partial torque with positive and negative n , resulting in NOT in some intervals of values in kR .

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Acknowledgments

This work is supported by Hong Kong RGC through HKUST2/CRF/11G and AoE/P-02/12. J.N. is also supported by RGC through HKBU604011 and HKBU603312. Z.L. is supported by NSFC through 11174059. J.C. is supported by Shanxi Science and Technology Department through 2014011008-1 and NSFC through 11404201.

Author contributions

All authors discuss the work thoroughly and extensively. J.C. performed the simulation, and assisted in physical analysis and analytical calculation. J.N. discovered the phenomenon of NOT and interpreted the physics. K.D. assisted in simulation, physical analysis, and analytical calculations. K.H.F. contributed to the initial conception of NOT. Z.F.L. developed the fundamental methodology and formalism. C.T.C. initiated the project and oversaw its progress.

Additional information

Supplementary information accompanies this paper at <http://www.nature.com/scientificreports>

Competing financial interests: The authors declare no competing financial interests.

How to cite this article: Chen, J. *et al.* Negative Optical Torque. *Sci. Rep.* **4**, 6386; DOI:10.1038/srep06386 (2014).



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